

5

10

**A CONTAINER, SUCH AS A FOOD OR
BEVERAGE CONTAINER, LUBRICATION METHOD**

15

20

Cross-Reference to Related Application

This application is a continuation-in-part of Application Serial No. 09/441,881,
filed November 17, 1999.

25

Field of the Invention

30

The invention relates to conveyor lubricants and lubricant compositions, and to
methods of use, for example, to treat or lubricate a container(s) and conveyor surfaces
or system for containers. The invention also relates to containers and conveyor surface
or system treated with a lubricant or lubricant composition. The container is, for
example, a food or beverage container.

35

Description of Related Art

Containers are receptacles in which materials are or will be held or carried.

Containers are commonly used in the food or beverage industry to hold food or

5 beverages. Often lubricants are used in conveying systems for containers, to ensure the appropriate movement of containers on the conveyor.

In the commercial distribution of many products, including most beverages, the products are packaged in containers of varying sizes. The containers can be made of paper, metal or plastic, in the form of cartons, cans, bottles, Tetra Pak™ packages,

10 waxed carton packs, and other forms of containers. In most packaging operations, the containers are moved along conveying systems, usually in an upright position, with the opening of the container facing vertically up or down. The containers are moved from station to station, where various operations, such as filling, capping, labeling, sealing, and the like, are performed.

15 Containers, in addition to their many possible formats and constructions, may comprise many different types of materials, such as metals, glasses, ceramics, papers, treated papers, waxed papers, composites, layered structures, and polymeric materials. Any desired polymeric material can be used, such as polyolefins, including polyethylene, polypropylene, polystyrene, and mixtures thereof, polyesters such as
20 polyethylene terephthalate (PET or PETE) and polyethylene naphthalate (PEN) and mixtures thereof, polyamides, polycarbonates, and the like.

Lubricating solutions are often used on conveying systems during the filling of containers with, for example, beverages. There are a number of different requirements that are desirable for such lubricants. For example, the lubricant should provide an
25 acceptable level of lubricity for the system. It is also desirable that the lubricant have a viscosity which allows it to be applied by conventional pumping and/or application apparatus, such as by spraying, roll coating, wet bed coating, and the like, commonly used in the industry.

In the beverage industry, it is also important that the lubricant be compatible
30 with the beverage so that it does not form solid deposits when it accidentally contacts spilled beverages on the conveyor system. This is important since the formation of

deposits on the conveyor system may change the lubricity of the system and could require shutdown of the equipment to facilitate cleaning.

It is also important that the lubricant can be cleaned easily. The container and/or the conveyor system may need to be cleaned. Since water is often in the cleaning solution, ideally the lubricant has some water-soluble properties.

Currently, containers, including polyethylene terephthalate (PET) bottles, and conveying systems for containers are often contacted with a volume of a dilute aqueous lubricant to provide lubricity to the container so that it can more easily travel down the conveyor system. Many currently used aqueous-based lubricants are disadvantageous because they are incompatible with many beverage containers, such as PET and other polyalkylene terephthalate containers, and may promote stress cracking of the PET bottles.

Furthermore, aqueous based lubricants are in general often disadvantageous because of the large amounts of water used, the need to use a wet work environment, the increased microbial growth associated with such water-based systems, and their high coefficient of friction. Moreover, most aqueous-based lubricants are incompatible with beverages.

Flooding a conveyor surface with a substantial proportion of aqueous lubricant typically occurs on food container filling or beverage bottling lines. Sufficient lubricant is used such that the lubricant is not retained entirely by the surface of the conveyor but tends to flow from the surface of the container, drip onto a conveyor support members and the surrounding environmental area around the conveyors. Further, sufficient amounts of lubricant are applied to the conveyor and other mechanisms of the plant under such conditions that a substantial foam layer of lubricant can form on the surface of the conveyor. As much as one inch (about 2.5 cm or more) thick of lubricant foam can contact a substantial portion of the base of a food container such as polyethylene terephthalate beverage bottle. We have found that current methods of lubricating such containers are wasteful of the lubricant material since a substantial proportion of the materials is lost as it leaves the container surface. Further, substantial proportions of the lubricant remain on the container and are carried from the conveyor as the food packaging or beverage-bottling operations are continued. A substantial need exists for

approved methods that waste little or no lubricant during packaging or bottling operations.

The tendency of polyester beverage containers to crack or craze is promoted by the presence of a number of common lubricating materials in contact with a substantial proportion of the surface of a polyester beverage container under pressure. The stress arises during manufacture of the polyester bottle from a preform. The stress is locked into the beverage container during manufacture and is often relieved as the lubricant materials contact the bottle. Lubricant materials appear to promote movement of the polyester molecules with respect to each other, relieving stress and leading to the creation of stress cracking. We have found that the degree of stress cracking is attributable, at least in part, to the amount of surface area of the bottle contacted by the lubricant. We have found in our experimentation that limiting the amount of surface area of the bottle that comes in contact with the lubricant can substantially improve the degree of stress cracking that occurs in the bottle material. Clearly, a substantial need exists to develop lubricating methods that result in the minimum amount of lubricant contact with the surface of the food container.

Summary of the Invention

We have found that the problems inherent in conventional aqueous lubrication of conveyor systems used in food packaging and beverage bottling can be substantially improved using a continuous thin film lubricant layer formed on a conveyor surface. The lubricant layer is maintained at a thickness of less than about 3 millimeters, preferably about 0.0001 to 2 mm, with an add on of lubricant on the surface of less than about 0.05 gms-in⁻², preferably about 5×10^{-4} to 0.02 gms-in⁻², most preferably about 2×10^{-4} to 0.01 gms-in⁻². Such a thin lubricating film of the lubricant on the conveyor provides adequate lubrication to the conveyor system but ensures that the lubricant cannot foam, does not flow from the conveyor surface and contacts the absolute minimum surface area of the food container such as the beverage bottle as possible. Such a thin film lubricant maintains significant lubrication while avoiding waste of the lubricant composition and avoiding stress cracking promotion. We have found that the preferred mode of formation of the liquid lubricant compositions of the invention are in

the form of an aqueous oil emulsion wherein the aqueous phase comprises about 10 to 50 wt% of the lubricant. The form of the emulsion can be either water in oil or oil in water emulsion. One preferred format of the emulsion is a phase unstable emulsion such that the emulsion separates forming an oil layer on top of a water layer which is then, in turn, contact with the conveyor surface. The methods of the invention can be used to convey virtually any food container on a conveyor line, but is particularly adapted to transporting both steel and aluminum cans and thermoplastic beverage containers such as polyethylene terephthalate beverage containers. Common PET beverage containers are formed with a pentaloid base having a five lobed structure in the base to provide stability to the bottle when it is placed on a surface. The contact with the lubricant on the pentaloid base must be minimized. We have found that using a thin film of emulsion lubricant, that less than about 10 to 300 mm², preferably 20 to 200 mm² of the surface of the bottle is contacted with lubricant. Certainly, the height of the lubricant in contact with the bottle is less than 3 millimeters. The motion of the conveyor, the tendency of the bottles to rock or move while being conveyed and the other aspects of relative movement at the bottle conveyor interface affect the height of the lubricant on the bottle. The methods of this invention are primarily directed to conveyor operations and do not involve any change in shape of the container arising from forming operations. The desirable coefficient of friction of the conveyor lubricant is about 0.1 to about 0.14.

The present invention provides in one aspect a container or conveyor for containers whose surface is coated at least in part with a thin, substantially non-dripping layer of a water-based cleaning agent-removable lubricant.

The invention also provides a process for lubricating a container, comprising applying to at least a part of the surface of the container a thin, substantially non-dripping layer of a water-based cleaning agent-removable lubricant.

The invention also provides a process for lubricating a conveyor system used to transport containers, comprising applying a thin, substantially non-dripping layer of a water-based cleaning agent-removable, substantially non-aqueous lubricant to a conveying surface of a conveyor, and then moving containers, such as beverage containers, on the conveyor.

The compositions used in the invention can be applied in relatively low amounts and with relatively low or no water content, to provide thin, substantially non-dripping lubricating films. In contrast to dilute aqueous lubricants, the lubricants of the invention provide drier lubrication of the conveyors and containers, a cleaner conveyor line and reduced lubricant usage, thereby reducing waste, cleanup and disposal problems.

Further features and advantages of the invention will become apparent from the detailed description that follows.

10 **Brief Description of the Drawings**

Figure 1 is a graphical representation of the friction data arising from the testing done with the Lubricant of Example 25.

15 **Detailed Description of Preferred Embodiments**

20 The present invention uses a thin, substantially non-dripping layer of a water-based cleaning agent-removable, substantially non-aqueous lubricant to lubricate containers and conveyor systems upon which the containers travel. By “substantially non-dripping”, we mean that the majority of the lubricant remains on the container or conveyor following application until such time as the lubricant may be deliberately washed away. By “water-based cleaning agent-removable”, we mean that the lubricant is sufficiently soluble or dispersible in water so that it can be removed from the container or conveyor using conventional aqueous cleaners, without the need for high pressure or mechanical abrasion. The phrase “substantially non-aqueous” means the lubricant is non-aqueous, includes water only as an impurity, or includes an amount of water that does not render the lubricant substantially non-dripping. When water is present in the lubricant, the amount of water preferably is less than about 50%, more preferably less than about 40% and most preferably about 5 to about 50 % by weight based on the weight of the lubricant.

25 A variety of materials can be employed to prepare the lubricated containers and conveyors of the invention, and to carry out the processes of the invention. For example, the lubricant can contain various natural lubricants, petroleum lubricants,

synthetic oils and greases. Examples of natural lubricants include vegetable oils, fatty oils, animal fats, and others that are obtained from seeds, plants, fruits, and animal tissue. Examples of petroleum lubricants include mineral oils with various viscosities, petroleum distillates, and petroleum products. Examples of synthetic oils include

5 synthetic hydrocarbons, organic esters, poly(alkylene glycol)s, high molecular weight alcohols, carboxylic acids, phosphate esters, perfluoroalkylpolyethers (PFPE), silicates, silicones such as silicone surfactants, chlorotrifluoroethylene, polyphenyl ethers, polyethylene glycols, oxypolyethylene glycols, copolymers of ethylene and propylene oxide, and the like. Examples of useful solid lubricants include molybdenum disulfide,

10 boron nitride, graphite, silica particles, silicone gums and particles, polytetrafluoroethylene (PTFE, Teflon), fluoroethylene-propylene copolymers (FEP), perfluoroalkoxy resins (PFA), ethylene-chloro-trifluoroethylene alternating copolymers (ECTFE), poly(vinylidene fluoride) (PVDF), and the like. The lubricant composition can contain an effective amount of a water-based cleaning agent-removable solid

15 lubricant based on the weight of the lubricant composition. The lubricant composition can also contain a solid lubricant as a suspension in a substantially non-aqueous liquid. In such a situation, the amount of solid lubricant can be about 0.1 to 50 weight percent, preferably 0.5 to 20 percent by weight, based on the weight of the composition. Also, the solid lubricant can be used without a liquid. In such a situation, the amount of solid

20 lubricant can be from about 50 to about 100 weight percent, preferably from about 80 to about 98 percent by weight, based on the weight of the composition.

Specific examples of useful lubricants include oleic acid, corn oil, mineral oils available from Vulcan Oil and Chemical Products sold under the "Bacchus" trademark; fluorinated oils and fluorinated greases, available under the trademark "Krytox" from is

25 DuPont Chemicals. Also useful are siloxane fluids available from General Electric silicones, such as SF96-5 and SF 1147 and synthetic oils and their mixture with PTFE available under the trademark "Super Lube" from Synco Chemical. Also, high performance PTFE lubricant products from Shamrock, such as nanoFLON M020™, FluoroSLIP™ 225 and Neptune™ 5031 and polyalkylene glycols from Union Carbide

30 such as UCON™ LB625, and Carbowax™ materials are useful.

The lubricants can be water-soluble but are preferably water-dispersible. In such cases, the lubricant can be easily removed from the container, if desired, by, for example, treatment with water. The lubricant, whether water-soluble or dispersible or not, is preferably easily removable from the container, conveyor and/or other surfaces in the vicinity, with common or modified detergents, for example, including one or more of surfactants, an alkalinity source, and water-conditioning agents. Useful water-soluble or dispersible lubricants include, but are not limited to, polymers of one or more of ethylene oxide, propylene oxide, methoxy polyethylene glycol, or an oxyethylene alcohol. Preferably the lubricant is compatible with the beverage intended to be filled into the container.

While many substantially non-aqueous lubricants are known per se, they have not been previously known or suggested to be used in the container or beverage container industries as described in this application. In certain embodiments, it is preferred that the lubricant is other than a (i) organic polymer, or other than a (ii) fluorine-containing polymer, or other than (iii) PTFE. In these embodiments, if (i), (ii) or (iii) is desired to be used, it can be used in combination with another lubricant.

The substantially non-aqueous lubricant used in the present invention can be a single component or a blend of materials from the same or different type of class of lubricant. Any desired ratio of the lubricants can be used so long as the desired lubricity is achieved. The lubricants can be in the form of a fluid, solid, or mixture of two or more miscible or non-miscible components such as solid particles dispersed in a liquid phase.

Also, a multistep process of lubricating can be used. For example, a first stage of treating the container and/or conveyor with a substantially non-aqueous lubricant and a second stage of treating with another lubricant, such as a substantially non-aqueous lubricant or an aqueous lubricant can be used. Any desired aqueous lubricant can be used, such as water. Any desired substantially non-aqueous lubricant can be used in the first or second stage. The lubricant of the second stage can be solid or liquid. By selection of appropriate first and second stages, desired lubrication can be provided. Also, the order of the second stage and first stage can be switched to give desired lubrication.

In addition to the lubricant, other components can be included with the lubricant to provide desired properties. For example, antimicrobial agents, colorants, foam inhibitors or foam generators, PET stress cracking inhibitors, viscosity modifiers, friction modifiers, antiwear agents, oxidation inhibitors, rust inhibitors, extreme
5 pressure agents, detergents, dispersants, foam inhibitors, film forming materials and/or surfactants can be used, each in amounts effective to provide the desired results.

Examples of useful antiwear agents and extreme pressure agents include zinc dialkyl dithiophosphates, tricresyl phosphate, and alkyl and aryl disulfides and polysulfides. The antiwear and/or extreme pressure agents are used in amounts to give
10 desired results. This amount can be from 0 to about 20 weight percent, preferably about 1 to about 5 weight percent for the individual agents, based on the total weight of the composition.

Examples of useful detergents and dispersants include alkylbenzenesulfonic acid, alkylphenols, carboxylic acids, alkylphosphonic acids and their calcium, sodium
15 and magnesium salts, polybutenylsuccinic acid derivatives, silicone surfactants, fluorosurfactants, and molecules containing polar groups attached to an oil-solubilizing aliphatic hydrocarbon chain. The detergent and/or dispersants are used in an amount to give desired results. This amount can range from 0 to about 30, preferably about 0.5 to about 20 percent by weight for the individual component, based on the total weight of
20 the composition.

Useful antimicrobial agents include disinfectants, antiseptics and preservatives. Non-limiting examples of useful antimicrobial agents include phenols including halo- and nitrophenols and substituted bisphenols such as 4-hexylresorcinol, 2-benzyl-4-chlorophenol and 2,4,4'-trichloro-2'-hydroxydiphenyl ether, organic and inorganic acids
25 and its esters and salts such as dehydroacetic acid, peroxycarboxylic acids, peroxyacetic acid, methyl p-hydroxy benzoic acid, cationic agents such as quaternary ammonium compound, aldehydes such as glutaraldehyde, antimicrobial dyes such as is acridines, triphenylmethane dyes and quinones and halogens including iodine and chlorine compounds. The antimicrobial agents can be used in an amount sufficient to provide
30 desired antimicrobial properties. For example, from 0 to about 20 weight percent,

preferably about 0.5 to about 10 weight percent of antimicrobial agent, based on the total weight of the composition can be used.

Examples of useful foam inhibitors include methyl silicone polymers. Non-limiting examples of useful foam generators include surfactants such as non-ionic,
5 anionic, cationic and amphoteric compounds. These components can be used in amounts to give the desired results.

Viscosity modifiers include pour-point depressants and viscosity improvers such as polymethacrylates, polyisobutylenes and polyalkyl styrenes. The viscosity modifier is used in amount to give desired results, for example, from 0 to about 30 weight
10 percent, preferably about 0.5 to about 15 weight percent, based on the total weight of the composition.

A layer of solid lubricant can be formed as desired, for example, by curing or solvent casting. Also, the layer can be formed as a film or coating or fine powder on the container and/or conveyor, without the need for any curing containers, including
15 polyethylene terephthalate containers, polymer laminates, and metal containers, such as aluminum cans, papers, treated papers, coated papers, polymer laminates, ceramics, and composites can be treated.

By container is meant any receptacle in which material is or will be held or carried. For example, beverage or food containers are commonly used containers.
20 Beverages include any liquid suitable for drinking, for example, fruit juices, soft drinks, water, milk, wine, artificially sweetened drinks, sports drinks, and the like. The lubricant should generally be non-toxic and biologically acceptable, especially when used with food or beverage containers.

The present invention is advantageous as compared to prior aqueous lubricants
25 because the substantially non-aqueous lubricants have good compatibility with PET, superior lubricity, low cost because large amounts of water are not used, and allow for the use of a dry working environment. Moreover, the present invention reduces the amount of microbial contamination in the working environment, because microbes generally grow much faster in aqueous environments, such as those from commonly
30 used aqueous lubricants.

The lubricant can be applied to a conveyor system surface that comes into contact with containers, the container surface that needs lubricity, or both. The surface of the conveyor that supports the containers may comprise fabric, metal, plastic, elastomer, composites, or mixture of these materials. Any type of conveyor system used in the container field can be treated according to the present invention.

Spraying, wiping, rolling, brushing, atomizing or a combination of any of these methods can be used to apply the liquid lubricant to the conveyor surface and/or the container surface. If the container surface is coated, it is only necessary to coat the surfaces that come into contact with the conveyor, and/or that come into contact with other containers.

Similarly, only portions of the conveyor that contacts the containers need to be treated. The lubricant can be a permanent coating that remains on the containers throughout its useful life, or a semi-permanent coating that is not present on the final container.

15

Examples

The invention can be better understood by the following examples. These examples are for illustration purposes only, and do not limit the scope of the invention.

In the examples, lubricity was measured as follows:

20

Lubricity test procedure:

Lubricity test was done by measuring the drag force (frictional force) of a weighted cylinder riding on a rotating disc, wetted by the testing sample. The material for the cylinder is chosen to coincide with the container materials, e.g., glass, PET, or aluminum. Similarly, the material for the rotating disc is the same as the conveyor, e.g., is stainless steel or plastics. The drag force, using an average value, is measured with a solid state transducer, which is connected, to the cylinder by a thin flexible string. The weight of the cylinder made from the same material is consistent for all the measurements.

30 The relative coefficient of friction (Rel COF) is calculated and used, where: Rel COF= COF(sample)/COF (reference) = drag force (sample)/drag force (reference).

Two commercially available aqueous-based lubricants for beverage conveyors were used as reference at recommended use dosage. They are reference 1= LUBODRIVE™ RX and reference 2= Lubri-Klenz™ LF; both are manufactured by Ecolab.

5 A Rel COF lower than 1 indicates a better lubricant than the reference. A good lubricant would have a typical Rel COF of less than 1.2, while a value greater than 1.4 would indicate a poor lubricant.

 The lubricity results of some non-aqueous based lubricants were tested and are shown below. The lubricity measurement was carried out with the method described
10 above. All the tests were using 100% of the stated materials or as indicated. The materials were either added or wiped onto the disc surface to result in a continuous film. The references were aqueous based lubricants and tested at 0.1% of conc. by weight in water for comparison. The test was run for several minutes until the force leveled off. The average drag force was recorded and the Rel COF was calculated based on the
15 average drag forces of the testing sample and the reference.

Example 1-3:

These examples demonstrated that corn oil, a natural oil, possesses lubricities which are better than or comparable to a commercially available aqueous based lube.

5 The cylinder material was mild steel for Example 1, glass for Example 2, and PET for Example 3. The rotating disk was stainless steel for Example 1-3.

	EXAMPLE 1		EXAMPLE 2		EXAMPLE 3	
	Mild steel-on stainless steel lubricity		Glass-on stainless steel lubricity		PET-on stainless steel lubricity	
	Corn oil	Refer. 1	Corn oil	Refer. 1	Corn oil	Refer. 1
Drag force (average) (g)	21.0	35.1	25.3	26.1	25.7	36.0
Rel COF	0.598	1.000	0.969	1.000	0.714	1.000

10

Example 4-6:

These examples demonstrated that Bacchus™ 22, a mineral oil, possesses lubricities which are better than the commercially available aqueous based lube. The cylinder material was mild steel for Example 4, glass for Example 5, and PET for example 6. The rotating disk was stainless steel for Example 4-6.

15

	EXAMPLE 4		EXAMPLE 5		EXAMPLE 6	
	Mild steel-on stainless steel lubricity		Glass-on stainless steel lubricity		PET-on stainless steel lubricity	
	Bacchus 22	Refer. 1	Bacchus 22	Refer. 1	Bacchus 22	Refer. 1
Drag force (average) (g)	10.2	31.3	22.4	27.6	18.6	31.1
Rel COF	0.326	1.000	0.812	1.000	0.598	1.000

Example 7-8:

These examples demonstrated that the two synthetic lubricants have a mild steel-on-stainless steel lubricity that is better than or comparable to the commercially available aqueous based lube. The cylinder material was mild and the rotating disk was stainless steel.

	EXAMPLE 7	EXAMPLE 8	
	Krytox GPL 100	Krytox GPL 200	Reference 1
Drag force (average) (g)	15.1	34.3	35.0
Rel COF	0.431	0.980	1.000

10 Example 9:

This example demonstrated that SF96-5, a synthetic siloxane lubricant, has a PET-on stainless steel lubricity that is better than the commercially available aqueous based lube. The cylinder material was PET and the rotating disk was stainless steel.

15

	SF96-5	Reference 1
Drag force (average) (g)	27.6	35.1
Rel COF	0.786	1.000

Example 10:

- 5 This example demonstrated that Krytox™ DF50, a solid lubricant in a solvent, possesses a mild steel-on stainless steel-lubricity that is comparable to the commercially available aqueous based lube. The cylinder material was mild steel and the rotating disk was stainless steel.

	Krytox DF50	Reference 1
Drag force (average) (g)	35.7	35.0
Rel COF	1.020	1.000

- 10 The sample was applied to the disc surface then the coating was wiped with an isopropanol-wetted towel and air dried to result in a very thin, smooth coating.

Example 11-12:

- 15 These examples demonstrated that behenic acid, a dry solid lubricant possesses a mild steel-on-stainless steel and glass-on-stainless steel lubricities which are comparable to a second commercially available aqueous based lube.

	EXAMPLE 11		EXAMPLE 12	
	Mild steel-on stainless steel lubricity		Glass-on stainless steel lubricity	
	Behenic acid	Reference 2	Behenic acid	Reference 2
Drag force (average) (g)	30.0	28.0	28.0	28.0
Rel COF	1.071	1.000	1.000	1.000

20

0.1% behenic acid in ethanol was applied to the stainless steel rotating disc. A thin dry film was formed after the solvent evaporation.

Example 13:

This example demonstrated that the Super lube oil with PTFE possesses a mild steel-on-stainless steel lubricity that is better than the commercially available aqueous based lube. The rotating disk was stainless steel.

	Super lube oil with PTFE	Reference 1
Drag force (average) (g)	27.9	33.2
Rel COF	0.840	1.000

Example 14-15:

These examples demonstrated that the mixture of oleic acid and Krytox GPL100 possesses mild steel-on-stainless steel and PET-on-stainless steel lubricities, which are better than the commercially available aqueous based lube. The ratio of oleic acid to Krytox GPL100 is about 1:1 by weight. The rotating disk was stainless steel.

	EXAMPLE 14		EXAMPLE 15	
	Mild steel-on stainless steel lubricity		PET-on stainless steel lubricity	
	Oleic acid/Krytox GPL100 (1:1)	Reference 1	Oleic acid/Krytox GPL100 (1:1)	Reference 1
Drag force (average) (g)	17.1	33.7	21.4	35.7
Rel COF	0.507	1.000	0.599	1.000

Example 16-17:

These examples demonstrate that the mineral oil, Bacchus 68 and its mixture with an antimicrobial agent, IRGASAN™ DP300 (2,4,4'-trichloro-2'-hydroxy-diphenyl-ether, obtained from Ciba Specialty Chemicals) possess a superior PET stress cracking resistance.

PET bottle stress cracking test:

31.0g of sodium bicarbonate and 31.0g of citric acid were added to a 2-liter PET bottle (manufactured by Plastipak) containing 1850g of chilled water and the bottle was capped immediately. The charged bottle was then rinsed with DI water and set on clear paper towel overnight.

Two testing liquids were prepared. Bacchus 68 was used as such as supplied. Bacchus 68 + 0.2% Irgasan DP300 was made by dissolving 1.0g of Irgasan DP300 in 500g of Bacchus 68 to result in a clear solution.

The base of the charged bottle was dipped into the testing liquid for 2-3 seconds then the bottle was placed in a plastic bag. The bottle with the bag was set in a bin and aged at 37.8°C and 90% humidity for 15 days. Four bottles were used for each testing liquid. The bottle was examined several times during the aging for bursting.

After the aging, the base of the bottle was cut off and examined for crazing and cracking. The results are listed in the table below.

The grading is based on a scale of A-F as:

- A: No signs of crazing to infrequent small, shallow crazes.
- B: Frequent small, shallow to infrequent medium depth crazes which can be felt with a fingernail.
- C: Frequent medium depth to infrequent deep crazes.
- D: Frequent deep crazes.
- F: Cracks, bottle burst before end of the 15 day testing.

Testing Liquid	PET STRESS CRACKING GRADING	
	EXAMPLE 16	EXAMPLE 17
	Bacchus 68	Bacchus 68 + 0.2% Irgasan DP300
Bottle 1	B	B
Bottle 2	B	B
Bottle 3	B	B
Bottle 4	B	B

Example 18:

This example demonstrates that the mineral oil, Bacchus 68 possesses a higher PET stress cracking resistance in contrast to the aqueous based beverage conveyor is lubricant, Lubodrive RX at a possible use dosage for conveyor lubrication.

The experimental procedure was the same as described in example 16-17 except that the testing liquid for Lubrodrive RX was 0.75% by weight in DI water. The charged bottle was placed in the plastic bag that contained 100g of the diluted Lubodrive RX. Also the experimental was carried out in the environmental oven at 37.8°C and 90% humidity for 13 days instead of 15 days.

The results showed that Bacchus 68 caused less stress cracking than the Lubodrive RX at 0.75%.

Example 19-20:

Example 19 demonstrates that the mineral oil, Bacchus 68, did not support the microbial growth, but killed the microbial in contrast to the commercially available beverage lube, Dicolube™ PL, manufactured by Diversey-Lever. Example 20 demonstrates that with the addition of the antimicrobial, methyl Paraben, to the mineral oil, the killing efficiency for the short time exposure was enhanced.

The Rate of Kill Antimicrobial Efficiency Test was carried out according to the method described below:

The bacteria, staphylococcus aureus ATCC6538 and enterobacter aerogenes ATCC 13048, were transferred and maintained on nutrient agar slants. Twenty-four hours prior to testing, 10 mls of nutrient broth was inoculated with a loopful of each organism, one tube each organism. The inoculated nutrient broth cultures were incubated at 37°C. Shortly before testing, equal volumes of both incubated cultures were mixed and used as the test inoculum.

For Dicolube PL, the lube was diluted to 0.5% wt with soft water. One ml of the inoculant was combined with 99 mls of the lubricant solution and swirled. For oil-

based lube, equal volumes of organisms were centrifuged at 9000 rpm 20°C for 10 minutes, then decanted and re-suspended in an equivalent volume of the mineral oil.

5 A one ml sample of the lubricant/inoculum mixture was removed after 5 minute exposure time and added to 9 mls of a sterile D/E neutralizing broth. The neutralized sample was serially diluted with buffered water and plated in duplicate using D/E neutralizing agar. The procedure was repeated after 15 and 60 minutes exposure times. The plates were incubated at 37°C for 48 hours then examined.

10 Controls to determined initial inoculum were prepared by adding one ml of inoculum to 9% mls of buffered water, serially diluting the mixture with additional buffered water, and plating with TGE.

The % reduction and log reduction were calculated as:

15
$$\% \text{ Reduction} = [(\# \text{ of initial inoculum} - \# \text{ of survivors}) / (\# \text{ of initial inoculum})] \times 100$$
 where: $\# \text{ of initial inoculum} = 3.4 \times 10^6 \text{ CFU/ml}$

CFU/ml: Colony forming units/ml

20
$$\text{Log Reduction} = [\log_{10} (\text{initial inoculum CFU/ml})] - [\log_{10} (\text{survivors inoculum CFU/ml})]$$

The table showed the results of Rate of Kill Test:

	EXAMPLE 19			EXAMPLE 20			COMPARISON EXAMPLE		
	Bacchus 68			Bacchus 68 w 0.05% methyl Paraben*			Dicolube PL		
Test Concentration	100%			100%			0.5% in DI water		
	Reduction			Reduction			Reduction		
Exposure time	No. of survivors CFU/ml	Log	Percent	No. of survivors CFU/ml	Log	Percent	No. of survivors CFU/ml	Log	Percent
5 minutes	2.4×10^5	1.15	92.941	8.6×10^4	1.60	97.470	3.5×10^6	NR**	NR
15 minutes	2.3×10^5	1.17	93.235	4.3×10^4	1.90	98.735	3.6×10^6	NR	NR
60 minutes	2.8×10^5	2.08	99.176	3.2×10^4	2.03	99.059	3.0×10^6	0.05	11.765

* Methyl Paraben: methyl 4-hydroxybenzoate, obtained 5 Chemicals Ltd.

5 ** NR: No reduction

Examples 21-22:

10 These examples demonstrate that behenic acid, a dry solid lubricant, in combination with a liquid lubricant provides a mild steel-on-stainless steel and glass-on stainless steel lubricities which are better than or comparable to the second commercially available aqueous based lube.

	EXAMPLE 21		EXAMPLE 22	
	Mild steel-on stainless steel lubricity		Glass-on stainless steel lubricity	
	Behenic acid, then H ₂ O	Reference 2	Behenic acid, then +H ₂ O	Reference 2
Drag force (average) (g)	26.0	28.0	25.0	28.0
Rel COF	0.929	1.000	0.893	1.000

0.1% behenic acid in ethanol was applied to the stainless steel disc, a thin dry film was formed after the solvent evaporation. H₂O was then applied to the surface of the dry film coated disc for the lubricity measurement.

- 5 The following table describes materials used in the above examples.

LUBRICANT MATERIAL/TRADE- NAME	MATERIAL INFORMATION	VENDOR
Bacchus 22	United States Pharmacopeia grade mineral oil	Vulcan Oil & Chemical Products
SF96-5	Polydimethylsiloxane	GE silicones
Krytox GPL 100	Perfluoropolyether	DuPont
Krytox GPL 200	Perfluoropolyether mixed with FIFE (Polytetrafluoroethylene)	DuPont
Krytox DF 50	Polytetrafluoroethylene in HCFC-14b	DuPont
Super lube oil with PTFE	Synthetic oil with PTFE	Synco Chemical
Oleic acid	Oleic acid	Henkel
Corn oil	Corn oil	

Examples 23-27

- 10 These examples use an oil in an aqueous emulsion and a glycerine stress
cracking inhibitor and an optional surfactant.

Example 23

Raw Material	% Weight
Glycerine (99.5% active)	72.7
Alkyl Poly Glyceride	2
Dow Corning HV495 Silicone Emulsion	2
DI Water	23.3

15

Example 24

Raw Material	% Weight
Glycerine (96% active)	75.7
Alkyl Poly Glyceride	2
Lambert E-2175 Silicone Emulsion	2
DI Water	20.3

Example 25

Emulsion

Raw Material	% Weight
Glycerine (96% active)	77.24
DI Water	20.71
Lambert E-2175 Silicone Emulsion	2.05

5

Example 26

Raw Material	% Weight
Glycerine (96% active)	77.95
DI Water	20.1
Mineral Seal Oil (White Oil)	4.95

Example 27

10

Raw Material	% Weight
Glycerin (96% active)	77.24
DI Water	20.71
Mineral Seal Oil (White Oil)	2.05

The product of example 25 was tested for COF and the results are as follows:

Lube (Ex. 25) Applied	COF	Lube Applied	Lub per unit area
g	unitless parameter	g	g.sq In
4	0.0846	4	0.002564
5	0.0717	5	0.003205
7	0.066	7	0.004487
10	0.0554	10	0.006410
15	0.0584	15	0.009615
20	0.0621	20	0.012821

Conveyor surface: 2 x 3.25" x 20 ft = 6.5" x 2012 = 1560 sq. In

15

Coefficient of friction (COF) measured on a short track conveyor system:
The determination of lubricity of the lubricant was measured on a short track conveyor system. The conveyor was equipped with two belts from Rexnord. The belt was

Rexnord LF (polyacetal) thermoplastic belt of 3.25" width and 20 ft long. The lubricant was applied to the conveyor surface evenly with a bottle wash brush. The conveyor system was run at a speed of 100 ft/min. Six 2L bottles filled with beverage were stacked in a rack on the track with a total weight of 16.15 kg. The rack was connected
5 to a strain gauge by a wire. As the belts moved, force was exerted on the strain gauge by the pulling action of the rack on the wire. A computer recorded the pull strength. The coefficient of friction (COF) was calculated on the basis of the measured force and the mass of the bottles and it was averaged from the beginning to the end of the run. The results of the testing of example 25 are shown in a graphical form in Fig. 1.

10 Applicants' invention can include aspects and embodiments, which are not herein specifically described. Accordingly this disclosure should not be read as being limited to the foregoing examples or preferred embodiments.